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Simulation of non-contact tonometer-Ocular response analyzer

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Abstract: As per World Health Organization, Glaucoma is considered as the second leading cause of irreversible blindness worldwide. An accurate assessment of Intraocular Pressure (IOP) is crucial for diagnosis and management of a chronic eye disease called Glaucoma. The elevation of IOP in eye leads to optic nerve damage and hence causing visual impairment. Thus, IOP measurement in tonometry has become an essential part of routine eye examinations for the diagnosis, screening and managing response to treatment in patients.

Simultaneous explosion of ophthalmic knowledge and medical instrument, being made in the 19th century, has led to the invention of tonometers of varied designs and principles, and Non-Contact Tonometers (NCTs) are among them. Glodmann Applanation Tonometer (GAT) is considered the 'gold standard' in measuring IOP; however, IOP measurement using GAT is now known to be affected by various factors like corneal thickness, curvature and material properties as demonstrated by Khan [1]. Due to inaccuracies in measuring IOP by GAT, this 'gold standard' has been challenged. Therefore, the present research aims to develop a multi-parametric correction equation to determine the True Intraocular Pressure (IOPT) using Non-Contact Tonometer and the current article focuses on evaluating the influence of individual parameters on IOP by NCT.

Keywords: Cornea, intraocular pressure, tonometry, glaucoma, numerical modeling.

1 Introduction

Glaucoma is a chronic eye disease caused by elevation in the Intraocular Pressure (IOP) of human eye and is stated to be the second leading cause of irreversible blindness worldwide, and around 66.8 million people are suspected to be victimised by the disease worldwide in the year 2000 [2]. Moreover, it is expected that the number of people affected by Glaucoma will increase considerably with the world's aging population. The fact that this disease doesn't show any major symptoms during its early development stages explains its criticality. The elevation of the IOP leads to optic nerve damage ultimately leading to visual impairment. Thus, IOP measurement has become an essential part of routine eye examinations for the diagnosis, screening and managing response to treatment in patients suffering from the said disease. Tonometer is a device which is used to gauge the IOP of the eye. The Goldmann Applanation Tonometer (GAT) is considered as the 'gold standard' for measuring IOP of the eye [3]. However, IOP measurement by GAT is now known to be affected by variations in central corneal thickness (CCT), curvature (R) and material properties of eye [4, 5, 6]. Due to such inaccuracies, its 'gold standard' has been challenged. While research is progressing to establish correction factors to improve IOP measurement by GAT [1], new tonometers of varying designs and principles have been developed with the aim of determining IOP estimates free from the variations in CCT, R and material properties; Non-Contact Tonometers (NCTs) are among them. The NCTs work on applanation principle similar to GAT. Different types of NCTs are available in the market popular among them are Ocular Response Analyzer (ORA: Reichert Corporation; Philadelphia, PA), Keeler PULSAIR (Keeler Ltd, Windsor, U.K), Reichert AT550 (Depew, NY, USA), Topcon CT60 (Topcon Corporation, Tokyo, Japan), Nidek NT4000 (Nidek Co. Ltd., Aichi, Japan) and Canon-TX10 (Canon USA Inc, One Canon Plaza, Lake Success, NY, USA). They use an air puff to create an applanation event on the human cornea. The change in the characteristics of the corneal light reflex produced by the air puff is measured electronically in NCTs. Unlike GAT, the main advantage of a NCT is that it requires no corneal contact; thereby decreasing the risk of disease transmission. Moreover, a NCT is patient friendly as no topical anesthesia is required in recording IOP.

Practical Significance. In a study by Martinez-de-la-Casa et al. [7], 48 eyes of 48 patients suffering from Glaucoma were examined using ORA & GAT. A mean difference of 7.2 mm Hg between GAT IOP and IOPG and a mean difference of 8.3 mm Hg between GAT IOP and IOGCC were recorded in the study. Thus, in both cases ORA measurement overestimated the GAT IOP. In another study by Kotecha et al. [8], 144 eyes of 144 untreated subjects were examined. In the study a factor termed 'Corneal Compensation Factor (CCF)' was introduced and the corresponding IOP was termed IOPCCF. The mean difference between GAT IOP and IOPCC on an average overestimated GAT IOP as found in the study. In another study by Lam et al. [9], 125 normal Chinese subjects were examined using ORA & GAT. The study demonstrated a better agreement between GAT and ORA than the previous two studies. A mean difference of just 0.33 mm Hg between IOPG and GAT IOP and 0.24 mm Hg between IOPCC and GAT IOP was established in the study. Therefore, preference is made that it should be ensured that IOP readings are taken using modern tonometers and factors affecting the IOP readings are recognised so that correct IOP measurement can be made.

The present study aims to develop a multi-parametric correction equation for determining True Intraocular Pressure (IOPT) using NCT. The correction equation can be developed by considering the simultaneous effect of variations in CCT, R and material properties. The study adopts a prudent methodology of predictive non-linear finite element numerical modeling to simulate the ORA procedure using ABAQUS software. Moreover, as a single equation, the correction equation is presented in a simple form suitable for clinical use.

2 Method

As outlined by Khan [1], many studies have been carried out in order to develop a correction equation for estimating true IOP by GAT independent of variations in corneal parameters like CCT, R and material properties. But sadly, not much of work has been done in analyzing the effect of these parameters on IOP measured by NCT. A parametric study will be conducted to gauge the effect various corneal parameters have on pressure measurements by NCT. The present study aims to improve the IOP estimation through NCT by developing a muti-paramateric correction equation which considers the simultaneous effect of variations in CCT, R and material properties; before which, the effect of individual parameters need to be accessed. The correction will be presented in a simple form suitable for clinical applications. In order to achieve this, representative non-linear finite element numerical simulation of the NCT procedure has been employed using ABAQUS software. The numerical models used in this study consider more realistic in-vivo behaviour of human eye like hyperelasicity, hysteresis and real- life cornea-sclera connection. Moreover, the findings of the parametric study are also clinically relevant as they will signify the importance of various corneal parameters and can give ophthalmologists an idea of the influence (if any) these parameters have on IOP measured by NCTs.

2.1 Finite element modeling using Abaqus

Numerical modeling based on non-linear finite element analysis has been used in the present study to enable a detailed representation of biomechanical behaviour of human cornea. Numerical modeling possesses the potential to represent realistic conditions without having to adopt the simplifications necessary with mathematical closed form solutions.



Parameter	Range of values considered in the study
CCT [mm] in steps of 100 μ m	0.445, 0.545, 0.645
Change in corneal radius R [mm] in steps of 0.6 mm	7.2, 7.8, 8.4
Hyperelasticity related to age	50-64 years, 65-79 years, 80-95 years
Change of Intraocular Pressure (IOP) [mm Hg]	10, 15, 20

Table 1: Parameter and corresponding range of values.

Human cornea possesses complex structure, both at the microscopic and macroscopic levels. Based on past research, the present study strikes the balance between cost and accuracy by distinguishing between the parameters that have a considerable effect and the parameters which can be ignored for their negligible effect on the corneal behaviour.

ABAQUS is the finite element package which has been employed in the present research for creating the numerical models and simulating the NCT procedure. ABAQUS VIEWER has been used to measure the deformations and reporting the behaviour of the corneal models. Applying symmetries in two planes along superior-inferior (vertical) and temporal-nasal (horizontal) directions, the FE model is shown in Fig. 1. The features like cornea's hyperselastic, hysteric and anisotropic behaviour, multi-layer construction, weak inter-laminar adhesion, non-uniform thickness, elliptical topography and connection to sclera have been optimised to improve the efficiency of the corneal models.

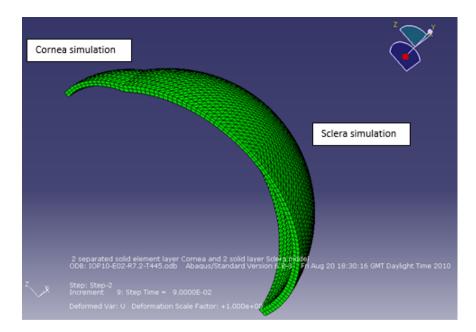


Fig. 1: FE simulation model of eye ball.

To conduct the parametric numerical study, a wide range of values for corneal thickness, curvature, age and IOP have been considered as summarised in Table 1.

Thus, in the present study altogether, 81 different Corneal Models have been generated for comparison.

Similar to Khan [1], the following stress (σ)-strain (ε) relationships handles the hyperelasticity within the material model, gathered through the testing of excised cornea tested for age range of 50 to 95 years old: $\sigma_{loading} \left(MPa \right) = 0.00480 \left(e^{64.8d\varepsilon} - 1 \right),$ (1)



where, $d = 1 - 0.0037 (87.5 - age_{years})$. (2) $\sigma_{unloading} (MPa) = 0.00036 (e^{355f\varepsilon} - 1)$, (3) where, $f = 1 - 0.0088 (87.5 - age_{years})$. (4)

2.2 Optimization for Developing the Correction Equation

In order to develop the multi-parametric correction equation, a Database Excel Sheet (Fig. 2) is formed containing the input values (CCT, R, Age and IOP) and the output values (P_1). With the use of Excel solver, the multi-parametric correction equation are put in the following form of single equation:

$$K = \frac{P_1}{IOPT} = A_{CCT}.A_R.A_{age}.A_{P_1}$$

where,

 $A_{CCT} = \text{effect of variation in CCT (mm)}$ $A_R = \text{effect of variation in R (mm)}$ $A_{age} = \text{effect of variation in age (years)}$ $A_{P_1} = \text{effect of variation in } P_1. \text{ (mm Hg)}$

3 Results

This section presents the findings of the parametric study that are conducted to analyse the effect of various corneal parameters on pressure measurements performed by NCT. In order to make an effort to accommodate the errors in tonometry readings subjected to the of variations in various corneal parameters; a multi-dimensional parametric study is conducted to assess the effects of variations in corneal thickness, curvature and age on the accuracy of first applanation pressure (P_1) measurement made by NCT within the ranges shown in Table 1.

To show the effect on material stiffness, the age range over which the numerical models are valid, that is 50-95 years, is further divided into three sub-ranges as follows-

-Young Age Range: 50-64 years with an average age = 57 years

-Middle Age Range: 65-79 years with an average age = 72 years

-Old Age Range: 80-95 years with an average age = 87.5 years

A numerical model with specific values of CCT, R, age and IOP are created for each case.

3.1 Effect of variation in CCT

The numerical estimation of the effect of CCT on P₁ measurement is shown in Fig. 3 for corneas with CCT ranging between 445 μ m and 645 μ m; age range is young, middle and old (average age = 57, 72 and 87.5 years respectively); and IOPT values of 10 mm Hg, 15 mm Hg and 20 mm Hg. The value of R is kept constant at a value of 7.8 mm in all cases. Fig. 3 shows a slightly non-linear increase in P₁ with higher CCT. This could be attributed to the fact that a close association exists between CCT and stiffness of cornea. Moreover, the relative error in pressure measurement is found to be affected by the IOPT level; for example, with CCT = 545 μ m and young age group (average age = 57 years), P₁/IOPT is 0.976, 0.656, and 0.497 under IOPT = 10 mm Hg, 15 mm Hg and 20 mm Hg respectively.

4	Α	B	С	D	E	F	G	н
1								
2		IOPT (mm Hg)	Are (years)	CCT (mm)	R (mm)	P1 (MPa)	P1 (mm Hz)	
3			- Be (Jeans)	()			(
4		10	57	0.445	7.2	0.001167	8.7525	
5		10	57	0.445	7.8	0.00114	8.55	
6		10	57	0.445	8.4	0.001126	8.445	
7		10	57	0.545	7.2	0.001356	10.17	
8		10	57	0.545	7.8	0.001301	9.7575	
9		10	57	0.545	8.4	0.00127	9.525	
10		10	57	0.645	7.2	0.001612	12.09	
11		10	57	0.645	7.8	0.001514	11.355	
12		10	57	0.645	8.4	0.001456	10.92	
13		10	72	0.445	7.2	0.001228	9.21	
14		10	72	0.445	7.8	0.001228	9.21	
15		10	72	0.445	8.4	0.001194	8.955	
16		10	72	0.545	7.2	0.001685	12.6375	
17		10	72	0.545	7.8	0.001477	11.0775	
18		10	72	0.545	8.4	0.001376	10.32	
19		10	72	0.645	7.2	0.002308	17.31	
20		10	72	0.645	7.8	0.001894	14.205	
21		10	72	0.645	8.4	0.001669	12.5175	
22		10	87.5	0.445	7.2	0.001442	10.815	
23		10	87.5	0.445	7.8	0.001442	10.815	
24		10	87.5	0.445	8.4	0.001353	10.1475	
25		10	87.5	0.545	7.2	0.002338	17.535	
26		10	87.5	0.545	7.8	0.001908	14.31	
27		10	87.5	0.545	8.4	0.001666	12,495	
28		10	87.5	0.645	7.2	0.003244	24.33	
29		10	87.5	0.645	7.8	0.002623	19.6725	
	н р	values Acct	Ar / Aage ;	Ap1 / P1	VECCT	P1 VeR	P1 Vs Age	Correc

(a) Database Excel Sheet

A	8	C	D	E	F	G	н	1	J	K	L	M	N	0	P
1															
2	IOPT (mm Hgj	Age (years)	CCT (mm)	R (mm)	P1 (MPa)	P1 (mm Hg)		Acct	Ar	Aage	Ap1	ĸ	IOPT	Error	Error2
4	10	57	0.445	7.2	0.001167	8.7525		0.636513	1.030828	0.677714	0.589971	0.914638	9.569357	-0.43064	0.18545
5	10	57	0.445	7.8	0.00114	8.55		0.636513	0.873374	0.677714	0.577072	0.891205	9.593747	-0.40625	0.16504
5	10	57	0.445	8.4	0.001126	8,445		0.636513	0.776547	0.677714	0.570387	3,786634	2.230213	-7.76979	60.369
7	10	57	0.545	7.2	0.001356	10.17		0.83885	1.030828	0.677714	0.680482	0.973415	10.44776	0.447758	0.20048
8	10	57	0.545	7.8	0.001301	9.7575		0.83885	0.873374	0.677714	0.654103	1.098804	8.880112	-1.11989	1.25414
9	10	57	0.545	8.4	0.00127	9.525		0.83885	0.776547	0.677714	0.63925	1.021055	9.328583	-0.67142	0.45080
10	10	57	0.645	7.2	0.001612	12.09		1.113241	1.030828	0.677714	0.803691	1.237539	9.769388	-0.23061	0.05318
11	10	57	0.645	7.8	0.001514	11.355		1.113241	0.873374	0.677714	0.756442	1.038428	10.9348	0.934797	0.87384
12	10	57	0.645	8.4	0.001456	10.92		1.113241	0.776547	0.677714	0.728527	1.027075	10.63213	0.632132	0.39959
13	10	72	0.445	7.2	0.001228	9.21		0.636513	1.030828	0.82734	0.619142	0.941781	9.779347	-0.22065	0.04868
14	10	72	0.445	7.8	0.001228	9.21		0.636513	0.873374	0.82734	0.619142	1.000687	9.203679	-0.79632	0.63412
15	10	72	0.445	8,4	0.001194	8.955		0.636513	0.776547	0.82734	0.602878	0.905987	9.884247	-0.11575	0.01339
16	10	72	0.545	7.2	0.001685	12.6375		0.83885	1.030828	0.82734	0.838953	1.230662	10.26886	0.26886	0.07228
17	10	72	0.545	7.8	0.001477	11.0775		0.83885	0.873374	0.82734	0.73863	1.02466	10.8109	0.810899	0.65755
18	10	72	0.545	8.4	0.001376	10.32		0.83885	0.776547	0.82734	0.690082	1.024284	10.07534	0.075335	0.00567
19	10	72	0.645	7.2	0.002308	17.31		1.113241	1.030828	0.82734	1.142223	1.86554	9.278816	-0.72118	0.52010
20	10	72	0.645	7.8	0.001894	14.205		1.113241	0.873374	0.82734	0.940228	1.517169	9.362834	-0.63717	0.40598
21	10	72	0.645	8.4	0.001669	12.5175		1.113241	0.776547	0.82734	0.83122	1.208974	10.35382	0.353818	0.12518
22	10	87.5	0.445	7.2	0.001442	10.815		0.636513	1.030828	1.107797	0.721794	0.999027	10.82553	0.825531	0.68150
23	10	87.5	0.445	7.8	0.001442	10.815		0.636513	0.873374	1.107797	0.721794	1.000152	10.81336	0.813359	0.66155
24	10	87.5	0.445	8.4	0.001353	10.1475		0.636513	0.776547	1.107797	0.679042	1.007297	10.07399	0.073987	0.00547
25	10	87.5	0.545	7.2	0.002338	17.535		0.83885	1.030828	1.107797	1.156932	1.735977	10.10094	0.100941	0.01018
26	10	87.5	0.545	7.8	0.001908	14.31		0.83885	0.873374	1.107797	0.947028	1.506097	9.501382	-0.49862	0.2486
27	10	87.5	0.545	8,4	0.001666	12.495		0.83885	0.776547	1.107797	0.82977	1.215716	10.27789	0.277893	0.07722
28	10	87.5	0.645	7.2	0.003244	24.33		1.113241	1.030828	1.107797	1.605695	2.340247	10.39634	0.39634	0.15708
19	10	87.5	0.645	7.8	0.002623	19.6725		1.113241	0.873374	1.107797	1.297148	1.967792	9.997244	-0.00276	7.6E-0

(b) Optimisation process

Fig. 2: Use of spread sheets to develop correction equations.

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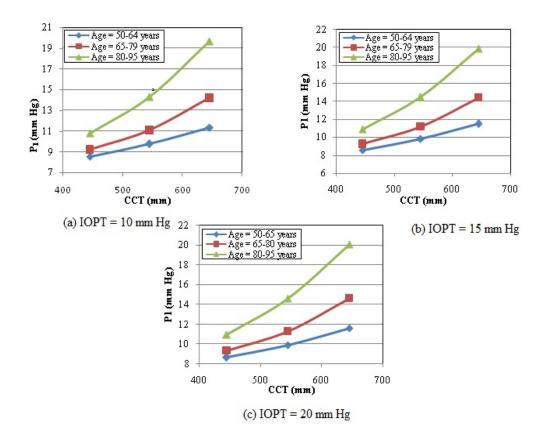


Fig. 3: Numerical estimation of the effect of CCT on P₁ measurement.

The average effect of variation on P₁ has been found to be 0.0145 mm Hg, 0.026 mm Hg and 0.0449 mm Hg per 1 μ m variation in CCT for corneas with young, middle and old age ranges respectively.

3.2 Effect of variation in R

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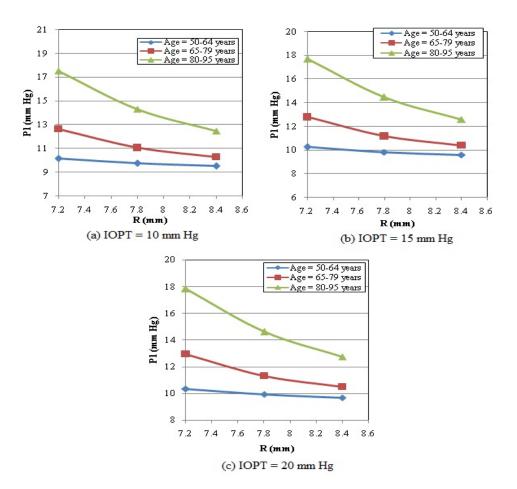
The numerical estimation of the effect of corneal curvature (R) on P₁ measurements is shown in Fig. 4 for corneas with R between 7.2 mm and 8.4 mm; age ranges of young, middle and old (average age = 57, 72 and 87.5 respectively); and IOPT values of 10 mm Hg, 15 mm Hg and 20 mm Hg. The value of CCT has been kept constant at a value of 545 μ m in all cases.

From Fig. 4 a consistent decrease in P_1 measurements with increasing R can be observed. This could be attributed to the fact that corneal stiffness decreases as the cornea gets flatter.

The average effect of R variation on P1 has been found to be 0.5451 mm Hg, 1.9833 mm Hg and 4.2229 mm Hg per 1 mm change in R for the young, middle and old age ranges respectively.

3.3 Effect of variation in age

Fig. 5 shows the numerical estimation of the effect of age on P₁ measurements by considering IOPs of 10 mm Hg, 15 mm Hg and 20 mm Hg. Each set of data includes three lines that correspond to CCT values of 445 μ m, 545 μ m and 645 μ m.



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Fig. 4: Numerical estimation of the effect of R on P₁ measurement.

The average increase in P₁ values has been found to be 0.7541 mm Hg, 1.515 mm Hg and 2.753 mm Hg per decade of age for corneas with CCT values of 445 μ m, 545 μ m and 645 μ m respectively.

4 Conclusion

From Fig. 3 it can be seen that for a given CCT, increase in age leads to increase in P₁ readings.

Moreover, the effect of R has been found to become more pronounced with the increase in age and could be attributed to higher material stiffness developed by cornea with increase in age.

Fig. 5 shows a nonlinear increase in P_1 measurements with increasing age and could be attributed to the age related material stiffness in cornea.

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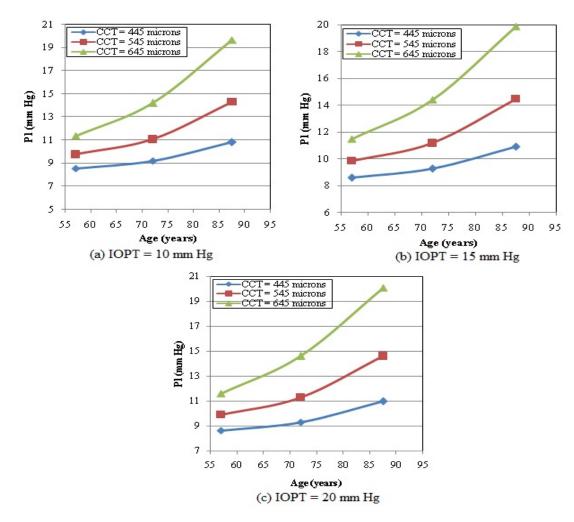


Fig. 5: Numerical estimation of the effect of age on P₁ measurement.

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